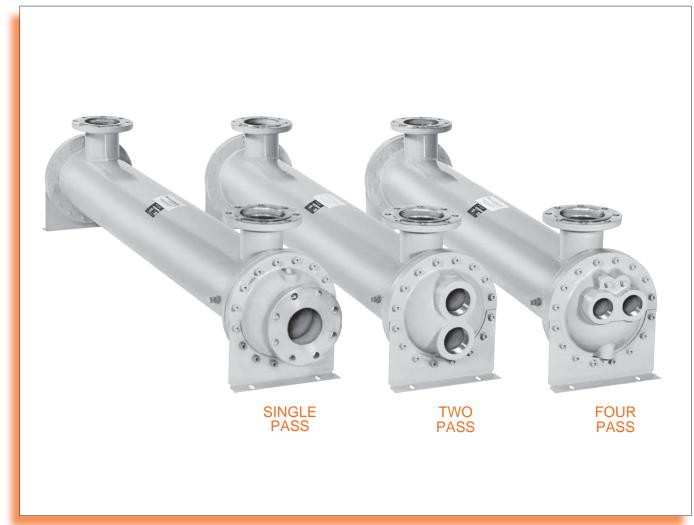


Manufacturer of Quality Heat Exchangers

AB2000 SERIES



Fixed Tube Bundle / Liquid Cooled

HEAT EXCHANGERS

- High thermal capacity.
- Large flow capacity.
- Operating pressure for tubes 150 PSI.
- Operating pressure for shell 300 PSI.
- Operating temperature 300 °F.

- Computer generated data sheet available for any application
- Can be customized to fit any applications.
- As an option, available in ASME code and certified

AB 2000 Series selection

STEP 1: Calculate the heat load

The heat load in BTU/HR or (Q) can be derived by using several methods. To simplify things, we will consider general specifications for hydraulic system oils and other fluids that are commonly used with shell & tube heat exchangers.

Terms	Kw = Kilowatt (watts x 1000)
GPM = Gallons Per Minute	T_{in} = Hot fluid entering temperature in °F
CN = Constant Number for a given fluid	$T_{out} = Hot fluid exiting temperature in °F$
ΔT = Temperature differential across the potential	$t_{in} = Cold fluid temperature entering in °F$
PSI = Pounds per Square Inch (pressure) of the operating side of the system	
MHP = Horsepower of the electric motor driving the hydraulic pump	$t_{out} = Cold fluid temperature exiting in °F$
The second	Q = BTU / HR

For example purposes, a hydraulic system has a 250 HP (186Kw) electric motor installed coupled to a pump that produces a flow of 200 GPM @ 2000 PSIG. The temperature differential of the oil entering the pump vs exiting the system is about 4.3°F. Even though our return line pressure operates below 100 psi, we must calculate the system heat load potential (Q) based upon the prime movers (pump) capability. We can use one of the following equations to accomplish this:

To derive the required heat load (Q) to be removed by the heat exchanger, apply ONE of the following. Note: The calculated heat loads may differ slightly from one formula to the next. This is due to assumptions made when estimating heat removal requirements. The factor (v) represents the percentage of the overall input energy to be rejected by the heat exchanger. The (v) factor is generally about 30% for most hydraulic systems, however it can range from 20%-70% depending upon the installed system components and heat being generated (ie. servo valves, proportional valves, etc...will increase the percentage required).

Formula	Example	Constant for a given fluid (CN)
A) $Q = GPM \times CN \times actual \triangle T$	A) $Q = 200 \text{ x } 210 \text{ x } 4 .3^{\circ}\text{F} = 180,600 \text{ btu/hr}$	Constant for a given find (Crv)
в) Q = [(PSI x GPM) / 1714] x (v) x 2545	в) Q =[(2000x200)/1714] x .30 x 2545 = 178,179 вти/нг	1) $O(1)$ $CN = 210$
c) $Q = MHP x (v) x 2545$	с) Q =250 x .30 x 2545 = 190,875 вти/нг	1) Oil $CN = 210$
D) $Q = Kw$ to be removed x 3415	d) $Q = 186 \text{ x} .30 \text{ x} 3415 = 190,557 \text{ btu/hr}$	2) Water
E) $Q = HP$ to be removed x 2545	е) Q =75 x 2545 = 190,875 btu/hr	3) 50% E. Glycol $CN = 450$

STEP 2: Calculate the Mean Temperature Difference

When calculating the MTD you will be required to choose a liquid flow rate to derive the Cold Side \triangle T. If your water flow is unknown you may need to assume a number based on what is available. As a normal rule of thumb, for oil to water cooling a 2:1 oil to water ratio is used. For applications of water to water or 50 % Ethylene Glycol to water, a 1:1 ratio is common.

$HOT FLUID \triangle T = Q$ Oil CN x GPM	EXAMPLE $\Delta \mathbf{T} = \frac{190,875 \text{ BTU/hr}}{210 \text{ CN x 200GPM}} (\text{from step 1, item c}) = 4.54^{\circ}\text{F} = \Delta \text{T} \text{ Rejected}$
$\begin{array}{ccc} \textbf{COLD FLUID} \bigtriangleup \mathbf{t} &= & \underline{BTU / hr} \\ \textbf{Water} & & \overline{CN \times GPM} \end{array}$	$\triangle t = \frac{190,875 \text{ BTU/hr}}{500 \text{ CN x 100GPM} (\text{for a } 2:1 \text{ ratio})} = 3.81^{\circ}\text{F} = \triangle t \text{ Absorbed}$
$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{ll} T_{in} &= 104.54 \ ^{\circ} F \\ T_{out} &= 100.0 \ ^{\circ} F \\ t_{in} &= 90.0 \ ^{\circ} F \\ t_{out} &= 93.81 \ ^{\circ} F \end{array}$
$\frac{\mathbf{T}_{out} - \mathbf{t}_{in}}{\mathbf{T}_{in} - \mathbf{t}_{out}} = \frac{\mathbf{S}[\text{smaller temperature difference}]}{\mathbf{L} [\text{larger temperature difference}]} = \left(\frac{\mathbf{S}}{\mathbf{L}}\right)$	$\frac{100.0^{\circ}\text{F} - 90.0^{\circ}\text{F} = 10.0^{\circ}\text{F}}{104.54^{\circ}\text{F} - 93.81^{\circ}\text{F} = 10.73^{\circ}\text{F}} = \frac{10.0^{\circ}\text{F}}{10.73^{\circ}\text{F}} = .931$

STEP 3: Calculate Log Mean Temperature Difference (LMTD)

To calculate the LMTD please use the following method; $LMTD_i = L \times M$ (L = Larger temperature difference from step 2.) x (M = S/L number (LOCATED IN TABLE A)) LMTD_i = 10.73 x .964 (FROM TABLE A) = 10.34

To correct the LMTD_i for a multipass heat exchangers calculate **R** & **K** as follows:

$$\mathbf{R} = \frac{\mathbf{T}_{in} - \mathbf{T}_{out}}{\mathbf{t}_{out} - \mathbf{t}_{in}} \qquad \mathbf{R} = \frac{104.54^{\circ}\text{F} - 100^{\circ}\text{F}}{93.81^{\circ}\text{F} - 90^{\circ}\text{F}} = \frac{4.54^{\circ}\text{F}}{3.81^{\circ}\text{F}} = \{\mathbf{1.191=R}\} \qquad \begin{bmatrix} \text{Locate the correction factor } CF_{\text{B}} \\ (\text{FROM TABLE B}) \\ \text{LMTD}_{\text{c}} = \text{LMTD}_{\text{i}} \times CF_{\text{B}} \\ \text{LMTD}_{\text{c}} = 10.34 \times .98 = \mathbf{10.13} \end{bmatrix}$$
$$\mathbf{K} = \frac{\mathbf{t}_{out} - \mathbf{t}_{in}}{\mathbf{T}_{in} - \mathbf{t}_{in}} \qquad \mathbf{K} = \frac{93.81^{\circ}\text{F} - 90^{\circ}\text{F}}{104.54^{\circ}\text{F} - 90^{\circ}\text{F}} = \frac{3.81^{\circ}\text{F}}{14.54^{\circ}\text{F}} = \{\mathbf{0.262=K}\}$$

TABLE E- Flow Rate for Shell &	Tube
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Бориции

Shell	Max.	Liquid	Flow	- Shel	Liquid Flow - Tube Side						
dia .		Baffl	e Spa	cing		S	P	٦	ΓP	F	۶P
Code	A	В	С	D	Е	Min.	Max.	Min.	Max.	Min.	Max.
2000	-	-	190	370	550	90	650	45	320	25	160

TABLE C										
U	TUBE FLUID	SHELL FLUID								
400	Water	Water								
350	Water	50% E. Glycol								
100	Water	Oil								
300	50% E. Glycol	50% E. Glycol								
90	50% E. Glycol	Oil								

AB 2000 Series selection

STEP 4: Calculate the area required

Required Area sq.ft. =

Q (BTU / HR) LMTD_c x U (from table C) $\frac{190,875}{10.13 \text{ x } 100} = 188.4 \text{ sq.ft.}$

STEP 5: Selection

a) From TABLE E choose the correct series size, baffle spacing, and number of passes that best fits your flow rates for both shell and tube side. Note that the tables suggest minimum and maximum information. Try to stay within the 20-80 percent range of the indicated numbers.

Example Oil Flow Rate = 200 GPM = Series Required from Table E = 2000 Series

Baffle Spacing from Table E

E = D baffle

Water Flow Rate = 100 GPM = Passes required in 2000 series = 4 (FP)

b) From TABLE D choose the heat exchanger model size based upon the sq.ft. or surface area in the series size that will accommodate your flow rate. Example

Required Area = 188.4 sq.ft Closest model required based upon sq.ft. & series = **AB-2007-D6-FP** If you require a computer generated data sheet for the application, or if the information that you are trying to apply does not match the corresponding information, please contact our engineering services department for further assistance.

TABLE A- FACTOR M/LMTD = L x M

S/L M		S/L	М	S/L	М	S/L	М	
	.01 .02 .03 .04	.215 .251 .277 .298	.25 .26 .27 .28 .29	.541 .549 .558 .566 .574	.50 .51 .52 .53 .54	.721 .728 .734 .740 .746	.75 .76 .77 .78 .79	.870 .874 .879 .886 .890
	.05	.317	.30	.582	.55	.753	.80	.896
	.06	.334	.31	.589	.56	.759	.81	.902
	.07	.350	.32	.597	.57	.765	.82	.907
	.08	.364	.33	.604	.58	.771	.83	.913
	.09	.378	.34	.612	.59	.777	.84	.918
	.10	.391	.35	.619	.60	.783	.85	.923
	.11	.403	.36	.626	.61	.789	.86	.928
	.12	.415	.37	.634	.62	.795	.87	.934
	.13	.427	.38	.641	.63	.801	.88	.939
	.14	.438	.39	.648	.64	.806	.89	.944
	.15	.448	.40	.655	.65	.813	.90	.949
	.16	.458	.41	.662	.66	.818	.91	.955
	.17	.469	.42	.669	.67	.823	.92	.959
	.18	.478	.43	.675	.68	.829	.93	.964
	.19	.488	.44	.682	.69	.836	.94	.970
	.20	.497	.45	.689	.70	.840	.95	.975
	.21	.506	.46	.695	.71	.848	.96	.979
	.22	.515	.47	.702	.72	.852	.97	.986
	.23	.524	.48	.709	.73	.858	.98	.991
	.24	.533	.49	.715	.74	.864	.99	.995

STANDARD CONSTRUCTION MATERIALS & RATINGS

Standard Model	AB-2000 Series	Standard Unit Ratings					
Shell	Steel	Operating Pressure Tubes					
Tubes	Copper	150 psig					
Baffle	Steel	Operating Pressure Shell 300 psig Operating Temperature					
Tube Sheet	Steel						
End Bonnets	Cast Iron						
Mounting Brackets	Steel	300 °F					
Gasket	Hypalon Composite						

Example Model

TABLE B- LMTD correction factor for Multipass Exchangers

	IAL	SLE	B- 1			orrec	ction	Tac	tori	or iv	iuitip	Jass	EXC	char	iger	5
		.05	.1	.15	.2	.25	.3	.35	.4	.45	.5	.6	.7	.8	.9	1.0
	.2	1	1	1	1	1	1	1	.999	.993	.984	.972	.942	.908	.845	.71
	.4	1	1	1	1	1	1	.994	.983	.971	.959	.922	.855	.70		
	.6	1	1	1	1	1	.992	.980	.965	.948	.923	.840				
	.8	1	1	1	1	.995	.981	.965	.945	.916	.872					
	1.0	1	1	1	1	.988	.970	.949	.918	.867	.770					
	2.0	1	1	.977	.973	.940	.845	.740								
	3.0	1	1	.997	.933	.835										
R	4.0	1	.993	.950	.850											
IX.	5.0	1	.982	.917												
T	6.0	1	.968	.885												
	8.0	1	.930													
	10.0	.996	.880													
	12.0	.985	.720													
	14.0	.972														
	16.0	.958														
	18.0	.940														
	20.0	.915														
•																

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TABLE D- Surface Area

Model	Surface Area in Sq.ft.									
Number	1/4" O.D	3/8" O.D	5/8 O.D							
Number	Tubing	Tubing	Tubing							
AB-2004	155.43	110.69	60.84							
AB-2005	194.29	138.36	76.05							
AB-2006	233.15	166.03	91.26							
AB-2007	272.00	193.70	106.47							
AB-2008	310.86	221.37	121.68							
AB-2009	349.72	249.04	136.88							
AB-2010	388.58	276.71	152.09							
AB-2011	427.43	304.38	167.30							
AB-2012	466.29	332.06	182.51							
AB-2013	505.15	359.73	197.72							
AB-2014	544.01	387.40	212.93							
AB-2015	582.86	415.07	228.14							

Options AB - 2008 - C 6 - TP - CNT - B - Z - Zinc Anode Z = 1 Zinc Anode Shell Diameter 2Z = 2 Zinc Anode etc. Model Baffle 2000 = 10.75" AB 2000 Effective Spacing Code Tubing Tube Length C = 4 1/2"Tube End Bonnets Blank = Copper (9" increments) Cooling Tube Side D = 9" Options Blank = Cast Iron Passes E = 18 " Diamenter CNT= 90/10 Cu Ni SP = 1 pass Options 4 = 1/4" STS = Stainless Steel TP = 2 pass 6 = 3/8" B = Bronze FP = 4 pass 10 = 5/8'SB = Stainless Steel

Instructions

The selection chart provided contains an array of popular sizes for quick sizing. It does not provide curves for all models available. Refer to page 14 & 15 for detailed calculation information.

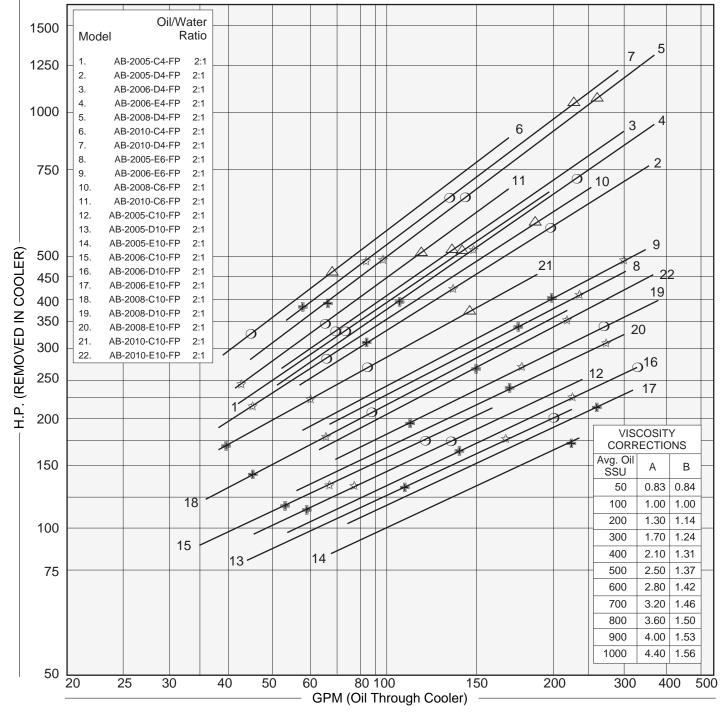
Computer selection data sheets for standard or special models are available through the engineering department of American Industrial. To use the followings graphs correctly, refer to the instruction notes "1-5".

- HP Curves are based upon a 40°F approach temperature; for example: oil leaving a cooler at 125°F, using 85°F cooling water (125°F - 85°F = 40°F).
- 2) The oil to water ratio of 1:1 or 2:1 means that for every 1 gallon of oil circulated, a minimum of 1 or 1/2 gallon (respectively) of 85°F water must be circulated to match the curve results.

- 4) Pressure Drop is based upon oil with an average viscosity of 100 SSU. If the average oil viscosity is other than 100 SSU, then multiply the indicated Pressure Drop by the corresponding value from corrections table A.
- 5) Corrections for approach temperature and oil viscosity are as follows:

$$H.P.(_{In Cooler}^{Removed}) = H.P.(_{Heat Load}^{Actual}) x (\frac{40}{Actual Approach}) x B.$$

HEAT ENERGY DISSIPATION RATES (Basic Stock Model)



AB 2000 Series dimensions

